GENERAL COMPUTATION PROGRAM

Introducing GCP — a New Program for Engineers — A Formula Solver

Requires only a limited degree of computer programming skill.

Problems are solved by the engineer in the traditional way:

- Write the formulas;
- 2) Enter the values of input parameters:
- The computer calculates the answers.

GCP requires that the formulas be written in BASIC code beginning with Program Line 100.

Four versions of GCP are listed herewith:

- A) PC-2 with printer
- B) PC-2 without printer
- C) PC-1 with printer
- D) PC-1 without printer

Keep GCP in the computer's memory so that the solutions to problems involving formulas may be quickly obtained. Before entry of new formulas, be sure the old formulas have been erased from memory. (To erase a program line, enter the line number while in the PRO mode, then press "Enter.") Use program lines 100-1200 in PC-2 (100-500 in PC-1).

After your formulas have been entered, you may, at your option, preserve the program on a cassette. In this way you can build up a library of customized GCP's. Of course, you may prefer to write the formulas into memory in PRO mode, each time the problem arises.

Example #1: SIMPLE RECTANGULAR BEAM

The Formula for Moment in a uniformly loaded simple beam is $1/8 \text{ wl}^2$.

For a rectangular beam, the Section Modulus equals 1/6 bd².

The flexural stress, f_b , equals the Moment divided by the Section Modulus, M/S.

The shear stress, f_V , equals $3/2 \cdot V/A$ where V = WI/2and A = bd

The input parameters are:

b (beam width, inches)

d (beam depth, inches)

w (load per foot)

I (span, feet)

These input parameters are assigned alphabetical designations, beginning with "!":

I = b = beam width, inches
J = d = beam depth, inches
K = w = load, lb/ft.
L = l = span, ft.

Output parameters are then assigned alphabetical designations beginning with "A". The formulas are rewritten in BASIC Code: (This should be quite easy for even those engineers who have never studied BASIC programming.)

becomes 100 A = K/8 * L \land 2 S = 1/6 bd² becomes 110 B = I/6 * J \land 2 f_b= 12 M/S becomes 120 C = 12 * A/B

 $M = 1/8 \text{ wl}^2$

 $f_{V}= 3/2 \text{ wl/(2 bd)}$ becomes 130 D = 3/2 * K * L/2/1/J or, alternatively 130 D = 3/2 * K * L/(2*|*J)

with the computer in the PRO mode, simply enter the line number (e.g. 100), followed by the formula, into the program. After each formula has been typed, press

"Enter". To check the formulas for correctness (PC-2), Type LL. 100, 130 and press "Enter" which will result in a printout of the formulas. On PC-1, you may type L. and press "Enter", and the entire program will be listed. The computer screen may of course be used to check for correctness.

To run the program press DEF A (Shift A on PC-1). Watch the display and follow the instructions.

To <u>rerun</u> the program, press DEF C (Shift C on PC-1). The rerun feature allows fast entry of new parameter values, with a minimum of wasted effort.

The answers are printed out in this order: A thru H. Thus, up to eight parameter values may be output.

NOTE: In Versions A and B of GCP (PC-2) you may, at your option, label the input and output parameters.

Example #2: PILE DRIVING INSPECTION

Determine the bearing value of the pile using the following dynamic formula for mechanical hammers:

$$R = \frac{2.5 E}{S+0.1} C$$

Where:

111

$$C = \frac{W_r + e^2 W_p}{W_r + W_p}$$

R = estimate of unit pile capacity, tons

S = the "set", i.e., the average penetration in inches per blow, for the last ten blows of the hammer, or alternatively, for the last foot of driving

E = driving energy, ft.-tons = W_r · h for single-acting hammers

 W_r = weight of ram, tons

h = height of fall, feet, single-acting hammers

 $W_D = Est.$ Weight of the pile, tons

0.65 phenolic laminate

0.55 steel on steel

0.5 hardwood blocks

0.25 softwood blocks

0 excessively soft packing or deteriorated blocks

The parameters S, W_p , W_r , e, E are entered as I, J, K, L and M. Note that the value of set, S, is not equal to I, but rather is a function of I. See below.

After the initial computation, only the values, I and J (weight of pile), need be entered to accomplish succeeding computations. (Enter I, press "Enter," then J, then press "Enter" twice. PC-2 only)

The formulas:

I = blows per foot, last foot (If the number of inches of penetration are measured for the last 10 blows, the formula becomes A = I/10)

110 B =
$$(K + L \land 2 * J)/(K + J)$$

120 C = $2.5 * M * B/(A + 0.1)$

Alternatively, if only the pile capacity is required, the last formula is assigned to A, thus:

120 A =
$$2.5 * M * B/(A + 0.1)$$

and the value, A, (pile capacity, tons) is the only output parameter.

Note The software provided in this issue is solely for educational and experimental purposes. It is supplied "as-is" without warranty of any kind. We do not assume any liability for any direct, indirect, incidental or consequential damages relating to the use or application of the programs or information contained herein.

> JIHZOX <u>(</u>)

Example #3: COLUMN DESIGN - MAIN MEMBERS

Ref: AISC "Manual of Steel Construction" (8th Ed., 1980). Design of a W, Tube or Pipe Column for Axial Load. Program solves:

- Rolled, or welded plate (built-up),
 H or I-shaped Columns, designated "W".
- 2) Pipe Columns, designated "P".
- 3) Tube (rectangular or square) Columns, designated "T".

Due to lack of memory capacity, PC-1 requires three programs so as to solve W, P, and T columns, respectively. We find that GCP in PC-1 will handle only about 10-15 program lines. Since the unaltered PC-2 has about 2K RAM, any GCP program which will work in PC-1 will, of course, also work in any PC-2. (Our PC-2 has the 8K RAM module.)

This is a trial-and-error design process. Therefore, set up a table of several trial sections, listing I_X , I_Y , A, d, b_f , t_f , F_Y .

The program:

- Calculates K_xl_x/r_xand K_yl_y/r_y; determines which is critical (larger).
- 2) If K1/r > 200, the program prints a message and stops.
- 3) For W columns, program checks flange width and, if necessary, calculates a reduction factor, $Q_{\rm s}$ where $Q_{\rm s} \leqslant 1$. See pp. 5-29, 5-30, and 5-94, AISC.
- 4) For Tube columns, program calculates ratio of width to thickness and, if necessary, calculates be (effective width) Using be, it calculates a reduction factor, Qa, where Qa≤1. See pp. 5-30 and 5-95, AISC.
- 5) For Pipe Columns, program checks thickness and, if necessary, calculates Fa(allowable axial stress in pipe where limited by diameter/thickness ratio). If pipe wall is too thin (diam/thickness too great) the program prints a message and stops.

6) Calculates C_C and the allowable axial stress, F_a, using either the CRC or Euler formula as appropriate. (Uses the Euler formula if KI/r exceeds C_C). See pg. 5-19 AISC. Formulas are modified by safety factor as discussed below. Note that F_a is modified by Q_a and Q_s as applicable. See Page 5-96.

Input Parameter Designations:

 $I = I_X$ (Mom. of Inertia, x, in-4)

J = ly (Mom. of Inertia, y, in. K = A (Cross-sect. Area, in. 2)

L = d (Depth of Member, in.), W section

M = bf (Flange Width, in.), W section

N = tf (Flange Thickness, in.), W section

O = F_V(Specified Min. Yield Stress, ksi)

P = P'(Applied Axial Load, kips)

Q = K_X(Effective Length Factor, x Direction)

R = Ky(Effective Length Factor, y Direction)

S = L_X(Length, Unbraced, x direction, Ft.)

T = Ly(Length, Unbraced, y Direction, Ft.)

For Tubes: L = depth of tube, in.

M = width of tube, in.
N = metal thickness, in.

For Pipes: L = M = Outside Diam, in.

N = metal thickness, in.

To determine values of K_X and K_V , see AISC Spec. para. 1.8, pp. 5-29 and 5-123 to 127; Table C-1.8.1, Pg. 5-124. Note that for braced frames, where the top and bottom of the column are maintained in alignment, Cases (a) or (b) of Table C-1.8.1 apply; however, for a pin-ended (Case d) column, K=1. We believe that designers should tend toward the use of K=1 because the possibility of imperfections of straightness and shape, because of out-of-plumbness or other accidental eccentricities of (non-axiality), and because of locked-in stresses within the metal associated, for example, with differential rates of cooling.

In cases where the frame is unbraced (sidesway not prevented), Cases (c), (e), and (f) of Table C-1.8.1 apply, and K > 1.

For continuous frames, see Alignment Chart, AISC pp. 5-125; however, for these cases, combined axial and bending loading will no doubt, be applicable. See February Issue!

The primary output parameters are 1) A = axial stress, f_a , and 2) B = allowable axial stress, F_a .

This program will be particularly useful for non-typical design situations, such as built-up columns, non-standard shapes, and where F_{γ} is not equal to 36 or 50 ksi.

Type these lines into the program, press DEF A (Shift A on PC-1) and follow the instructions in the display.

Line 100 allows user to designate which type of column cross-section (W, P, or T) is to be designed. Line 110-130 calculates two values of kl/r, selects larger value, and determines whether kl/r exceeds 200. If so, program stops.

Lines 140-180 are for W columns. Checks unstiffened flange-thickness ratio ($\frac{1}{2}$ of the flange width, divided by flange thickness) to determine whether a stress reduction factor, V (Q_S), is required. If so, calculates V.

```
140: IF U$\(\)"W"THEN 200
150: IF M/2/N\(=95/\)(0)^.5THEN 200
160: IF M/2/N\)176/\(\)
0)^.5THEN 180
170: V=1.415-.00437
*M/2/N*O^.5:
GOTO 200
180: V=20000/\(0*\)(0*\)
```

Lines 200-240 are for tube columns, square or rectangular. Calculates Z (b_e) and if Z is less than the maximum tube width, calculates stress reduction factor, W (Q_a).

Lines 300-330 are for pipe columns. Calculates diam/thickness ratio (L/N) and if too large, calculates maximum working stress, F_a ; it will stop the program if ratio is larger than $13000/F_V$.

Lines 400-410 calculate $C_{\rm C}$ (E); then if kl/r (C) is greater than $C_{\rm C}$, the Euler formula is used to calculate $F_{\rm a}$ (F), modified by safety factor 23/12. If not, the CRC formula is used, modified by a variable safety factor. Line 420 accounts for the case where a value of $F_{\rm a}$ (D) was calculated for a pipe column, in line 320.

```
380: [F U>1LET U=1
390: IF W>1LET W=1
400:E=(58E3*Π*Π/(U
    *W*0))^.5: IF C
    >ELET F=12*π*π
    *29E3/(23*C*C)
    :GOTO 420
410:F=(1-C*C/2/E/E
    )*0:F=F/(5/3+3
    \8*C\E-C*C*C\8
    /E^3)
420: IF X=1AND F>D
    LET F=D
430: X=E: E=C: B=F*U*
    W: A=P/K: D=F*K*
    U*W: C=P:F=X
450: IF BKAPRINT "C
    OL. OVERSTRESSE
    D''
```

GCP Listings (PC-1) W Columns

```
110:A=QS*12/(I/K
                       170: V=1.415-.004
                           37M/2/N*0^.5
    >^.5:B=RT*12
    ∠(J∠K)^.5:V=
                           :GOTO 380
                       180:V=20000/(0*(
120:C=A:IF B>C
                           M/2/H)^2)
    LET C=B
                       380:IF V>1LET Y=
130:IF C>200
PRINT "KL/R>
                       400:E=(2Л^2*29E3
    200: INVALID"
                           ∠(VO))^.5:IF
    :PRINT " ":
                           C>ELET F=12π
    PRINT " ":
                           ^2*29E3/(23*
    G0T0 555
                           C^2):GOTO 42
150:IF M/2/N<=95
    /0^.5THEN 38
                       410:F=(1-CC/2/E/
                           E)*0#F=FZ(5Z
160:IF M/2/N>176
                           3+3/8*C/E-CC
    70^.5THEN 18
                           CZ8ZE^3)
                      420:X=E:E=C:B=FV
                           :A=P/K:D=FKV
                           :C=P:F=X
       Tube Columns
110:A=12QSZ(IZK)
                       180: W = (Z + H) / (Y + H)
    ^.5:B=12RT/(
    J/K)^{.5:W=1}
                       380:IF W>1LET W=
120:C=A:IF B>C
    LET C=B
                       400:E=(X*X*58E3/
130: IF C>200
                           (WO))^.5: IF
    PRINT "KL/R>
                           C>ELET F=12II
    200:INVALID"
                           *II*29E3/(23C
    :PRINT " ":
                           C):GOTO 420
    PRINT " ":
                       410:F=(1-CC/2/E/
    G0T0 555
                           E)*0:F=F/(5/
150:Y=L:H=M:IF M
                           3+3/8*C/E-CC
    >YLET Y=M:H=
                           CZ8ZE^3)
                       420:X=E:E=C:B=FW
160:IF Y/N<=238/
                           :A=P/K:D=FKW
    0^.5THEN 380
                           *C=P*F=X
170:Z=253N/(P/K)
    ^.5*(1-50.3/
    ((Y/N)*(P/K)
    ^.5)):IF Z>Y
    LET Z=Y
       Pipe Columns
110:A=QS*12/(I/K
                       170:D=662/L*M+.4
    )^.5#B=RT*12
                           *0:X=1
    /(J/K)^.5:X=
                       400:E=(2Π^2*29E3
    0
                           /0)^.5:IF ()
120:C=A:IF B>C
                           ELET F=12\pi^2
    LET C=B
                           *29E3/(23*C^
130:IF C>200
                           2):60T0 415
    PRINT "KL/R>
                       410:F=(1-CC/2/E/
    200: INVALID"
                           E)*0:F=F/(5/
```

POCK

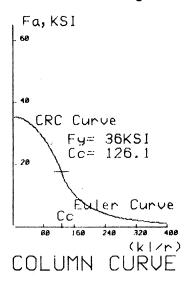
GRAPHICS

The enclosed listing permits plotting of the CRC-Euler curve; a unique curve is plotted for each yield stress.

The length of the ordinate scale is appropriate for F_y values up to about 65 ksi; this could of course be modified within the program for greater values of F_y .

This curve represents the estimated buckling failure stress, versus kl/r. It is apparent from a study of this curve why kl/r values greater than 200 are not deemed prudent.

For main members with kl/r values greater than $C_{\rm C}$, the required safety factor is 23/12; for members with kl/r equal to $C_{\rm C}$ or less, the CRC curve is used, modified by a safety factor varying from 5/3 at kl/r=0, to 23/12 at kl/r= $C_{\rm C}$.



This compound curve is based on experience and actual performance of steel columns during testing and research. Obviously, steel cannot be stressed at a higher level than F_y (yield stress). Therefore the curve intersects the ordinate at F_y . It was found that the CRC curve approximates the experimental data; the Euler Curve is valid at kl/r values higher than C_c (C_c equals kl/r at $F_y/2$).

3+3/8*C/E-CC

A=P/K:D=FK:C

C787E^3)

415:IF X=1IF F>D

420:X=E:E=C:B=F:

LET F=D

=F:F=X

:PRINT " ":

PRINT " ":

/OTHEN 400

ZOPRINT "INV

ALID COLUMN" :GOTO 555

G0T0 555

150:IF L/N<=3300

160: IF L/N>13000

NEWS

 \subseteq

()

Sharp apparently intends to replace PC 1211 (Radio-Shack's PC-1) with their new PC-1250, PC-1211. an upgrade of Enhanced BASIC, better handling of strings, and two-dimensional arrays will be among the features of this improved pocket unit. Possibly faster-not sure. Price? Probably about \$110. A thermal printer peripheral, with micro cassette recorder built in, will sell for about \$170. Our comment: Sounds good, but a larger RAM than 2K sure would have been nice!

PROGRAMMERS TIP .

Use your PC-2 as an <u>electric typewriter</u>. Types with automatic return. Variable type size (Csize 1-4). However, watching it type "vertically" takes some getting used to!

Note the use of INKEY to assign letters, numbers, etc. to A\$. The computer "waits" in line 9020 until something (letter, number, etc.) is typed. Also note the use of ASC in lines 9030 and 9040 to convert A\$ to a number for purposes of line shifting, so that you may use the "up" and "down" arrows (ASC numbers 10 and 11, resp.) to change lines. Line 9110 shifts up, and line 9120 shifts down. Use the arrow key on the printer to start a new "page". For rapid repeats, hold the key down.

Suggestion: add this short routine to the end of certain programs to permit custom-typing of a message. To activate, press DEF=. When done, press BREAK (ON).

9000: "="GRAPH: INPUT "CSIZE ?(1-4)"; A:CSIZE A:ROTATE 1:GLCURSOR (190,0):SORGN

9005: B=INT (80/A+.4)

9010: FOR X=0 TO B

9020: V\$=INKEY\$:IF V\$="" THEN 9020

9030: IF ASC V\$=10 THEN 9110

9040: IF ASC V\$=11 THEN 9120

9050: LPRINT V\$:V\$="":NEXT X

9110: GLCURSOR (-10*A,0):SORGN: GOTO 9010

9120: GLCURSOR (10*A,0):SORGN:GOTO

9010

9999: END

PC-1 Owners: If you have bought Radio Shack's "Civil Engineering" software, take note of an error in the Section Properties program ("SECT") as follows:

Line 199: A=D-C:E=-E:GOTO 185 should be: A=D-C:E=-E:C=-C:GOTO 185 which corrects the calculation of Radius of Gyration of Symmetric Box, I, or C Section.

GENERAL NOTES

We would enjoy hearing from you.We want our efforts to be responsive to your needs in Civil Engineering practice. purpose, as we see it, is to help you become more efficient in your engineering work through the use of the computer. To us, the computer is a "means to an end". the "end" being more efficiency and more accuracy - a higher plane of engineering practice. We think the portable units have a distinct advantage over the non-portable. If you have a contribution to make, for example, a program to submit, please do No mailings returned. Cliff Hall. Editor, CECOM, P.O. Box 6. Hart. MI 49420.

NEXT ISSUE

The February Issue will present the complete AISC analysis procedure GCP programming for Combined Axial and Bending of Steel Members using PC-2. For PC-1/PC-2 users we will use GCP to solve wood foundation walls using National Forest Products Association (NFPA) procedure.

CASSETTES

We offer cassette tapes with documentation at \$20 each for:

- 1) Statistics-Confidence Program PC-1
- 2) Statistics-Confidence Program PC-2
- 3) GCP with or without Printer PC-1
- 4) GCP with or without Printer PC-2
- 5) Accounts Receivable PC-2*

*This program prints detailed invoices. Prepares summary of business during the time period. Suitable for a small engineering office (up to five hourly categories of charge rates).

Listing - GRAPHICS COLUMN CURVE

00) 4: INPUT "Fy, KSI= "; FY: SORGN :

GLCURSOR (0, -2

3:/'A"CLEAR

GRAPH :

CSIZE 1 6:LINE -(0, 260): LINE (0,0)-(20)0,0)

7:FOR I=80TO 240 STEP 80: GLCURSOR (0, 1) :RLINE(0,0)-(5,0):LPRINT 1/ 4: NEXT I

8: FOR 1=40TO 200 STEP 40: GLCURSOR (1,0) RLINE(0,0)-(0, 4)

9: GLCURSOR (I-9, -10):LPRINT 2* I:NEXT I

10:L1=0:F1=FY

13: CSIZE 2

14:CC=π*(2*29E3/F Y > 0.5

15: GLCURSOR (3, 26 0):LPRINT " Fa ,KSI";GLCURSOR (150, -30): LPRINT "(kl/r) ":GLCURSOR (CC /2,0):RLINE (0 ,0)-(0,6)

16:GLCURSOR (CC/2 -5, 10): LPRINT "Cc": GLCURSOR (CC/2-10, FY*2) :RLINE(0,0)-(20, 0): GLCURSOR

(CC/2+10, FY*3) 12:LPRINT "Fy=";F Y; "KSI"; GLCURSOR (CC/2 +10, FY*3-18): LPRINT "Cc="; INT (CC*10+.5) 110

19:GLCURSOR (CC/4 -3.7*FY): LPRINT "CRC Cu nve"; GLCURSOR (.65*CC, 25); LPRINT "Euler Curve" 20:GOTO 35

30:L1=L2

35:L2=L1+2.5: (F L 2>400THEN 80 37: IF ZZ=1THEN 50

40:F2=FY*(1-.5*(L 1/00)^2): 11 1-2 <=FY/2LET ZZ-1 -GOTO 50

45:GOTO 60

50: F2=π^2*29E3/L2 ^2

60:LINE (L1/2, F1* 4)-(L2/2, F2*4)

20:F1=F2:GOTO 30 80: TEXT : LF 3: GRAPH : CSIZE 3 :LPRINT "COLUM

> N CURVE" TEXT CSIZE 2:LF 6

999: END

10: "A"CLEAR 20:BEEP 4:PAUSE ### I-T " 25:BEEP 2: INPUT

30: I\$="I": J\$="J

T"

35:FOR A=9TO 8+ A(53)

40:A\$(A+26)=A\$(A):NEXT A

67:A(54)=0:GOTO 70

):NEXT A

70:BEEP 2:FOR A INPUT A(A):

NEXT A 75: IF A(54)=1THEN 90

"AVAIL:8 OUT MS?";A(55)

__LATION"

Listing - GCP (PC-1 with printer)

"*****GCP*** **":PAUSE "I NPUT PARAMS: "# INPUT PAR AMS?(12MAX)" (53) ": K\$="K" 31:L\$="L":M\$="M ": N\$="N": O\$=

"0":P\$="P":Q \$="Q":R\$="R" :S\$="S":T\$="

69:"C"PAUSE "GC P-RERUN":A(5 4)=1:FOR A=9 TO 8+A(53):A \$(A)=A\$(A+26

=9T0 A(53)+8 : PAUSE "INPU T":PAUSE A#(A);"..";A\$(A);"..";A\$(A) ;"..";A\$(A):

80:BEEP 2:PAUSE

PUT PARA: A-H ":BEEP 2: INPUT "NO.OF OUTPUT PARA 90: PAUSE "CALCU

501:BEEP 2:PRINT GEN COM P GM":PRINT "

RESULTS" 503:FOR A(56)=1 TO A(55):A(A (56)+26)=A(A (56)): NEXT A (56)

504:A\$="A=":B\$=" B=":C\$="C=": D\$="D=":E\$=" E=":F\$="F="

507:G\$="G=":H\$=" H="

510:FOR A(56)=1 TO A(55): PRINT A\$(A(5 6))

520:PRINT A(A(**56**)+26)

530:NEXT A(56): PRINT " "

540:FOR A(56)=9 TO A(53)+8: PRINT A(A(56)):NEXT A(56

550:PRINT " ": PRINT " ": PRINT " "

555: INPUT "RERUN ?PRESS SHFT 0"3Z

560: END

Listing - GCP (PC-2 with printer)

```
8: "A"WAIT 70:
   CLEAR
 9: PRINT "GENERAL
    COMPUTATION P
   GM"
10: REM
11: REM
          PROGRAM
    INSTRUCTIONAL
    MESSAGE
12: REM
13:LS$="**
        **"
   **
15: IM$=:"N": INPUT
   "INSTRUCTION M
   SG?(Y/N)"; IM$
16: IF IMS="N"THEN
   25
17: PRINT "BEFORE
   RUNNING, BE SU
   RE"
18: PRINT "FORMULA
   S ARE ENTERED"
19: PRINT "LINES 1
   00 THROUGH 120
   9"
20: PRINT "AT YOUR
    OPTION, LABEL"
22: PRINT "TITLE &
    INPUT PARAMET
   ERS"
25: PRINT "ENTER A
    PGM TITLE"
27. INPUT "PROGRAM
    TITLE=":PT$
30:0$(10)="J":0$(
   11)="K":@$(9)=
   " 1 "
31:0$(12)="L ":0$
   (13)="M":Q$(1)
   4)="N ":@$(15)
   ="0 ":0$(16)="
   P ":0$(17)="Q
32:@$(18)="R ":@$
   (19)="S ":@$(2
   0)="T ":Q$(21)
   ="U ":@$(22)="
   U ":@$(23)="W
33: @$(24)="X ":@$
   (25)="Y":0$(2
   6)="Z"
```

```
35:@$(1)="A ":@$(
   2) = "B ": Q$(3) =
   "C ":@$(4)="D
   "; Q$(5)="E "
37: Q$(6)="F ": Q$(
   7)="G ":@$(8)=
   "H "
40: REM
41: RFM
       ENTER
   INPUT PARAMS
42: REM
50: PRINT "PROVIDE
    LBLS FORK# 18
    PARAMS"
53: PRINT "ENTER T
   HE INPUT PARAM
   SII
54: INPUT "NO. INPU
   T PARAMS="; ZZ
56: IF ZZ>18PRINT
   "ERROR": GOTO 5
57: PRINT "ENTER P
   ARAM LABELS"
58: PRINT "IN THIS
    ORDER: 1-Z"
59:WAIT 5
60:FOR 11=9TO ZZ+
   8:CLS :FOR 12=
   2TO 22STEP 2:
   CURSOR 12:
   PRINT @$(11):
   NEXT 12: INPUT
   @$(11):NEXT 11
61:WAIT 50:GOTO 6
62: "C"SK=1: WAIT 5
65: PRINT "GIVE VA
   LUES TO PARAMS
70: FOR 11=9TO ZZ+
   8:PRINT Q$(II)
   : INPUT @(II):
   NEXT II
71: REM
72: REM
         ENTER AND
    LABEL OUTPUT
   PARAMETERS
23: REM
```

```
74: D1$="N": INPUT
    "DOCUMENTATION
    ? (Y/N)";DI$
 75: IF SK=1THEN 87
 76: PRINT "ENTER O
    UTPUT PARAMS"
 77: INPUT "NO.OUTP
    UT PARAMS=": YY
 78: IF YY>8PRINT "
    ERROR": GOTO 26
 80: PRINT "ENTER O
    UTPUT PARAM LB
    LS A-H"
83:WAIT 5
84: FOR 11=1TO YY:
    CLS :FOR 12=2
    TO 22STEP 2:
    CURSOR 12:
    PRINT @$(II):
    NEXT 12: INPUT
    @$(II):NEXT II
85:WAIT 100
87: LPRINT : LPRINT
    PT$:LPRINT LS$
    :LPRINT : IF DI
    $="N"THEN 95
90:FOR II=9TO ZZ+
   8:LPRINT @$(II
   );" = ":LPRINT
   @(II):NEXT II
93: LPRINT
95: REM
96: REM
        CARRY OUT
    CALCULATIONS:
   PGM LINES 100-
   1200
97: REM
1203: REM
1204: REM
         PRINT
     OUTPUT
```

```
1240; NEXT II
1245:LF 1
1247: REM
1248: REM INSTRUC-
     TIONAL MSG
1249: REM
1250: PRINT "DEF C
      FOR NEW PRO
     B":LPRINT
1272: IF DI$="N"
     THEN 1970
1275: GOTO 1990
1970:FOR II≈9TO Z
     Z+8:LPRINT @
     (11)
1980: NEXT II
1990:LF 3
9999: END
```

1220:FOR II=1TO Y Y 1230:LPRINT @\$(]]

);" = ": LPRINT @(II)

Listing - GCP (PC-2 without printer)

_
8:"A"WAIT 70: CLEAR
9:PRINT "GENERAL COMPUTATION P
GM" 10: REM
11:REM PROGRAM INSTRUCTIONAL
MESSAGE 12:REM
15: IM\$="N": INPUT "INSTRUCTION M
SG?(Y/N)"; IM\$ 16: IF IM\$="N"THEN 30
17: PRINT "BEFORE
RE" 18: PRINT "FORMULA S ARE ENTERED" 19: PRINT "LINES 1
19: PRINT "LINES 1 00 THROUGH 120
20: PRINT "AT YOUR
OPTION, LABEL" 22: PRINT "INPUT P ARAMETERS"
30:Q\$(10)="J":Q\$(11)="K":Q\$(9)=
31:Q\$(12)="L ":Q\$ (13)="M ":Q\$(1 4)="N ":Q\$(15) ="O ":Q\$(16)=" P ":Q\$(17)="Q
32:Q\$(18)="R ":Q\$ (19)="S ":Q\$(2 0)="T ":Q\$(21) ="U ":Q\$(22)=" U ":Q\$(23)="W
33:@\$(24)="X ":@\$ (25)="Y ":@\$(2
6)="Z " 35:Q\$(1)="A ":Q\$(2)="B ":Q\$(3)= "C ":Q\$(4)="D
":@\$(5)="E " 37:@\$(6)="F ":@\$(7)="G ":@\$(8)=
"H "

```
41 REM ENTER
    INPUT PARAMS
 42: REM
 50: PRINT "PROVIDE
     LBLS FOR<= 18
     PARAMS"
 53: PRINT "ENTER T
    HE INPUT PARAM
    SII
 54: INPUT "NO. INPU
    T PARAMS="; ZZ
 56: IF ZZ>18PRINT
    "ERROR": GOTO 5
    3
 57: PRINT "ENTER P
    ARAM LABELS"
 58: PRINT "IN THIS
     ORDER: 1-Z"
 59:WAIT 5
 60:FOR II=910 ZZ+
    8:CLS :FOR I2=
    2TO 22STEP 2.
    CURSOR 12:
    PRINT @$(]1):
    NEXT 12: INPUT
    @$(II):NEXT II
 61:WAIT 90:GOTO 6
 62: "C"SK=1:WAIT 9
 65: PRINT "GIVE VA
    LUES TO PARAMS
 70: FOR II=9TO ZZ+
    8: PRINT @$(II)
    :INPUT @(II):
    NEXT II
 71: REM
 72: REM
         ENTER AND
     LABEL OUTPUT
    PARAMETERS
123: REM
 75: IF SK=1THEN 97
 26: PRINT "ENTER O
    UTPUT PARAMS"
 77: INPUT "NO.OUTP
    UT PARAMS="; YY
 78: IF YY>8PRINT "
    ERROR": GOTO 76
 80: PRINT "ENTER O
```

UTPUT PARAM LB

LS A-H"

83:WAIT 5 84:FOR II=1TO YY 85:CLS :FOR I2=2 TO 22STEP 2:
CURSOR 12: PRINT @\$(11): NEXT 12:INPUT @\$(11):NEXT 11 90:WAIT 90
95:REM 96:REM CARRY OUT CALCULATIONS: PGM LINES 100- 1200
97:REM 1203:REM 1204:REM PRINT OUTPUT
1205:REM 1210:PRINT "COMP. RESULTS:"
1215: PRINT "PRESS ENTER TO DI
SPLAY ANS" 1220: "FOR II=1 TO YY: WAIT 8
1230: PRINT @\$(II)
1235:WAIT :PRINT @(II) 1240:NEXT II:WAIT
1240:NEXT II:WAIT 150:PRINT "R EDISPLAY ANS WERS?DEF SPA CE"
1250: PRINT "PRESS DEF C FOR R
ERUN" 1260:WAIT :PRINT "INPUT REVIE W?PRESS ENTE R"
1270:FOR II=9TO Z Z+8:PRINT @(II):NEXT II
9999: END

40: REM

Listing	-	GCP	(PC -1	without	printer;)

10:"A"CLEAR 20:BEEP 4:PAUSE	e V
"*****GCP*** **":PAUSE "I	
NPUT PARAMS:	
NPUT PARAMS: *** I-T" 25:BEEP 2:INPUT	-
"# INPUT PAR AMS?(12MAX)"	
;A(53) 30:I\$="I":J\$="J	-
":К\$≔"К"	, C.C.
31:L\$="L":M\$="M ":N\$="N":O\$=	
"O":P\$="P":Q \$="Q":R\$="R"	
:S\$="S": T\$= " T"	5
35:FOR A≕9TO 8+	
A(53) 40:A\$(A+26) =A\$(5
Α):NEXT Α 67:A(54)=O:GԾΤԾ	5
70 69:"C"PAUSE "GC	
P-RERUN":A(5 4)=1:FOR A=9	C
TÜ 8+A(5 3): A	5
\$(A)=A\$(A+26):NEXT A	5
70:BEEP 2:FOR A =9TO A(53)+8	
:PAUSE "INPU T":PAUSE A≸(5
A);"";A\$(A	
);"";A\$(A) ;"";A\$(A): INPUT A(A):	
INPUT A(A): NEXT A	
75:IF A(54)=1 THEN 90	
80:BEEP 2:PAUSE "AVAIL:8 OUT	
PUT PARA:A—H	
":BEEP 2: INPUT "NO.OF	
OUTPUT PARA MS?";A(55)	

90:PAUSE "CALCU LATION"

-1 v	vitho	out	prii	nt er
501:	PAU ESU PRI ESU FN	LTS NT	": "F0 PR	RR
503:	FOR (56 (56 (56	A(A(5)+2)):)	56) 5): 6)= NEX	A(A A(A T A
504:	A\$= B=" D\$= E="	:C\$ "D=	="C " : E	=": \$="
507:	5 ‡= H="	"G=	":H	\$="
510:	" "(=1T(PAU(6))	J A SE	(55 A\$(): A(5
520:	0+26	5)		
530:	NEXT PRIN PLA' T SH	ΓΑ YT ΥΑΙ	"RE	DIS
532:	PRIM PPRE C"	4T		
535:	PRIM REV S EM	YTE!	W?PI R"	RES
540 :	FOR TO # PRIM)):M	4(5) 4T i	3)+: A(A	3 : (56

SAMPLE RUNS (PC-1 and PC-2) W 14X43 Column, 28 ft. long

STEEL COLUMN	GEN COM PGM
** ** ** **	RESULTS
MOM INERT X = 428 MOM INERT Y = 45.2 AREA = 12.6 MEM DEPTH, IN = 13.66 MEM WIDTH, IN = 7.995 FLG [-NESS, IN = 0.53 YIELD STR, KSI = 36 APPLIED LOAD, K = 59 KX = 1 COL.LGTH.X, FT = 28 COL.LGTH.Y, FT =	A= 4.682539683 B= 4.745046668 428. 45.2 12.6 13.66 7.995 0.53 36. 59. 1. 28. 28.

28

COMP. RESULTS:

AXIAL STRESS, KSI =

ALLOW AX STRESS, =

4.682539683

4.745046668